



RF operation of AlN/Al_{0.25}Ga_{0.75}N/AlN HEMTs with f_T/f_{max} of 67/166 GHz

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We report on highly-scaled Al_{0.25}Ga_{0.75}N channel high electron mobility transistors. Regrown ohmic contacts covering the sidewall of the compressively strained Al_{0.25}Ga_{0.75}N channel exhibited a low contact resistance of $R_c = 0.23 \Omega \cdot \text{mm}$. Scaled devices with a T-shaped gate showed record high speed for any AlGa_N-based transistors, $f_T/f_{max} = 67/166$ GHz, while simultaneously achieving high average breakdown field exceeding 2 MV cm^{-1} . The load-pull measurements performed at 10 GHz revealed a 20% peak power added efficiency with an output power density of 2 W mm^{-1} , which is mainly limited by the RF dispersion. © 2023 The Japan Society of Applied Physics

AlGa_N channel high electron mobility transistors (HEMTs) show potential for next-generation high-power RF applications with the promise of a high Johnson's figure of merit ($\text{JFOM} = V_{br} \times f_T$) compared to the incumbent Ga_N HEMT technology.^{1–3)} Therefore, it is critical to increase the device's three-terminal off-state breakdown voltage V_{br} while ensuring a high unit gain cutoff frequency f_T in order to achieve superior RF performance. Previous theoretical studies have suggested that the saturation velocity v_{sat} of AlGa_N alloys is comparable to Ga_N, while possessing a wider energy bandgap.^{2,4,5)} This indicates that for equivalent device dimensions, the maximum achievable f_T^{max} in HEMTs, which is determined by the ratio of saturation velocity to gate length, should be similar for AlGa_N and Ga_N channels. With a higher breakdown field and similar saturation velocity, AlGa_N channel transistors are therefore expected to deliver higher power density at high frequencies.

While it might seem intuitive to maximize the Al content in the AlGa_N channel HEMTs for superior RF performance due to higher breakdown voltage, such consideration has to be balanced with other design concerns.⁶⁾ For example, when the Al content increases, the low-field mobilities and carrier densities in the AlGa_N channel decrease, increasing the sheet resistance and, as a result, the parasitic delay, thereby reducing f_T and f_{max} . Moreover, it becomes difficult to make ohmic contacts to the AlGa_N channel as the Al concentration of AlGa_N grows.^{7–12)} So, an optimal Al mole fraction of the AlGa_N channel needs to be chosen that simultaneously maximizes f_T , f_{max} , and V_{br} to demonstrate an improvement over the conventional Ga_N HEMT technology.

Although AlGa_N channel transistors are making rapid progress in long-channel devices designed for power-switching applications, there are limited reports of their RF performance. Xue et al.¹³⁾ reported a record f_T/f_{max} of 40/58 GHz for Al_{0.75}Ga_{0.25}N/Al_{0.6}Ga_{0.4}N HEMTs. The highest output power of Al-rich AlGa_N to date, 2.7 W mm^{-1} at 10 GHz albeit at a low power-added efficiency (PAE) of 4%, was achieved in microchannel Al_{0.65}Ga_{0.35}N/Al_{0.4}Ga_{0.6}N HFET structures.¹⁴⁾

In this study, we report a highly scaled T-gated Al_{0.25}Ga_{0.75}N quantum well channel HEMT (QW HEMT), for improved RF performance. We demonstrate devices with simultaneously high I_D^{max} ($>900 \text{ mA mm}^{-1}$) with low Ron

($=6.5 \Omega \cdot \text{mm}$), high average breakdown field strength ($>2 \text{ MV cm}^{-1}$) and record high $f_T/f_{max} = 67/166$ GHz for AlGa_N channel HEMTs. We demonstrate high average breakdown voltage without any field plate technique, which could potentially provide cost advantages for high-voltage RF applications.

The AlN/Al_{0.25}Ga_{0.75}N/AlN QW HEMTs presented in this study were grown on semi-insulating 6H-SiC substrates by plasma-assisted molecular beam epitaxy. The as-grown heterostructure consists of a $1 \mu\text{m}$ AlN buffer layer, a 24 nm Al_{0.25}Ga_{0.75}N channel, and a 15 nm AlN barrier. Further details on epitaxial growth are presented in Ref. 15. Nanometrics HL5500 Hall measurement system was used to characterize the as-grown sample. With soldered corner indium contacts to the 2DEG at the top AlN/AlGa_N interface, a charge density and electron mobility of $3.05 \times 10^{13} \text{ cm}^{-2}$ and $45 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ were measured, respectively.

The fabrication process used for the QW HEMTs in this study is an extension of the process presented in Ref. 6. To explore the RF performance of AlN/AlGa_N/AlN HEMTs, an electron beam lithography (EBL) defined T-shaped gate was introduced in place of a rectangular gate previously defined by photolithography, and a Si₃N₄ passivation layer was added for an improved dispersion control. A tri-layer resist stack was patterned by EBL, and a Schottky contact was formed by sputtering 10 nm Ni and e-beam evaporating 300 nm Au. The HEMTs were then passivated with 100 nm plasma-enhanced chemical vapor deposition Si₃N₄. Figures 1(a) and 1(b) show the final HEMT cross-section and a scanning electron microscope (SEM) image of a T-gate, respectively. The reported HEMTs feature a source-to-drain spacing $L_{SD} = 600 \text{ nm}$, $W_G = 2 \times 25 \mu\text{m}$ device width, and a T-shaped gate placed in the middle of the source-to-drain spacing with a gate length $L_G = 70 \text{ nm}$.

The DC characterization of the HEMTs was done using a Keithley 4200 parameter analyzer. After the device fabrication, a contact resistance from the top metal pad to 2DEG (R_c) and a sheet resistance (R_{sh}) were extracted by the linear transfer length method. The extracted $R_{sh} = 4.66 \text{ k}\Omega \text{ sq}^{-1}$ closely matches with that measured on the as-grown sample via Hall-effect, indicating minimum process damage. The regrown n+ Ga_N non-alloyed ohmic contacts exhibited $R_c = 0.23 \Omega \cdot \text{mm}$, which is the lowest contact resistance to 2DEG among all AlGa_N channel HEMTs reported in the

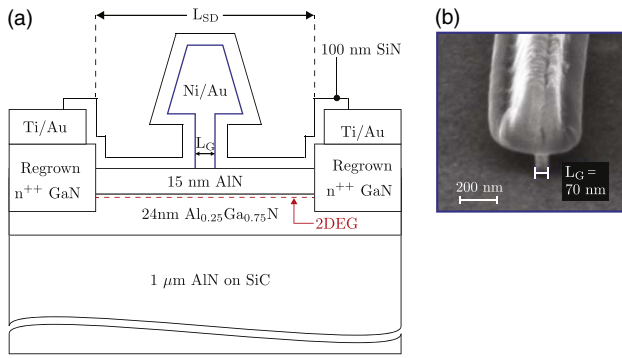


Fig. 1. (a) Cross-sectional representation of the fully processed AlN/Al_{0.25}Ga_{0.75}N/AlN HEMTs with a T-shaped gate. (b) SEM image of a 70 nm T-shaped gate cross section.

literature.^{2,16} Figures 2(a) and 2(b) show the transfer curves measured at a drain bias $V_{DS} = 5$ V, revealing an on/off ratio exceeding 10^6 with sharp pinch-off characteristics and a peak transconductance $g_m = 0.11$ S mm⁻¹. The output curves in Fig. 2(c) show a maximum drain current $I_D = 0.9$ A mm⁻¹ at a gate bias $V_{GS} = 2$ V and an on-resistance $R_{on} = 6.5$ Ω · mm. The observed DC output conductance (G_{DS}) is higher than that of previously reported AlN/GaN/AlN HEMTs with a similar gate length,^{17,18} suggesting the presence of short channel effects (SCE). The cause of SCE is most likely a thicker AlN barrier used in this study, resulting in a low channel aspect ratio (L_G/d , d = gate-to-channel distance) less than 4.5.¹⁹ Further supported by negligible G_{DS} observed in AlGaN channel HEMTs with a longer gate length on the same chip,⁶ where we previously reported the details on the epitaxy and low-field transport in AlGaN channel HEMT structures, the short channel effect is expected to be suppressed upon thinning down the top AlN barrier.

To investigate the dynamic and transient behavior, pulsed I - V measurements were performed using 4225-PMU modules with a Keithley 4200 parameter analyzer. 500 ns long pulses and a 1 ms period were used, and the drain current density at $V_{GS} = 0$ V, -4 V, and -9 V was pulsed from

different biasing conditions, (V_{GSq} , V_{DSq}) = (0 V, 0 V), (-10 V, 0 V), and (-10 V, 10 V), to assess current collapse and knee walkout. The AlGaN channel HEMTs demonstrated appreciable RF dispersion, with an average of $\sim 10\%$ current collapse [shown in Fig. 3(a)]. The possible sources of current dispersion include the surface states and a formation of a two-dimensional hole gas or a filling of hole traps located near the valence band edge at the bottom GaN/AlN interface with a net negative polarization charge.^{20,21} To suppress RF dispersion in future devices, a proper control of surface states with an in situ passivation layer and a Si- δ doping in the AlN back barrier to compensate positive charges may be necessary.²²

RF characterization was performed using an Agilent 8722ES network analyzer and Infinity GSG probes. After the short-open-load-through calibration, scattering parameters were measured in the frequency range of 100 MHz to 40 GHz, and parasitic elements were de-embedded using on-wafer open and short structures. f_T and f_{max} were extracted from scattering parameters by extrapolating $|h_{21}|^2$ and a unilateral gain U , respectively, following the -20 dB dec⁻¹ slope. As shown in Fig. 3(b), the HEMTs biased at (V_{GS} , V_{DS}) = (-4 V, 10 V) for maximum transconductance demonstrated a record high $f_T/f_{max} = 67/166$ GHz for any AlGaN channel HEMTs.

To explore the potential for high-frequency applications, sub-micron channel lengths were examined for breakdown. The three-terminal off-state breakdown voltage was measured by increasing V_{DS} until breakdown of the HEMT occurred with the gate voltage set below the threshold voltage, $V_{GS} \sim -10$ V. The breakdown voltage metric used in this study is defined as the drain voltage at which the drain current (I_D) exceeds 1 mA mm⁻¹. Figure 4(a) shows the three-terminal off-state breakdown of three AlGaN QW channel HEMTs with varied gate-drain distances. Among all devices, a breakdown voltage of 59 V was measured for a HEMT with a 260 nm gate-drain distance. This corresponds to an average breakdown field exceeding 2 MV cm⁻¹. Figure 4(b) shows the scaling of breakdown voltage as a

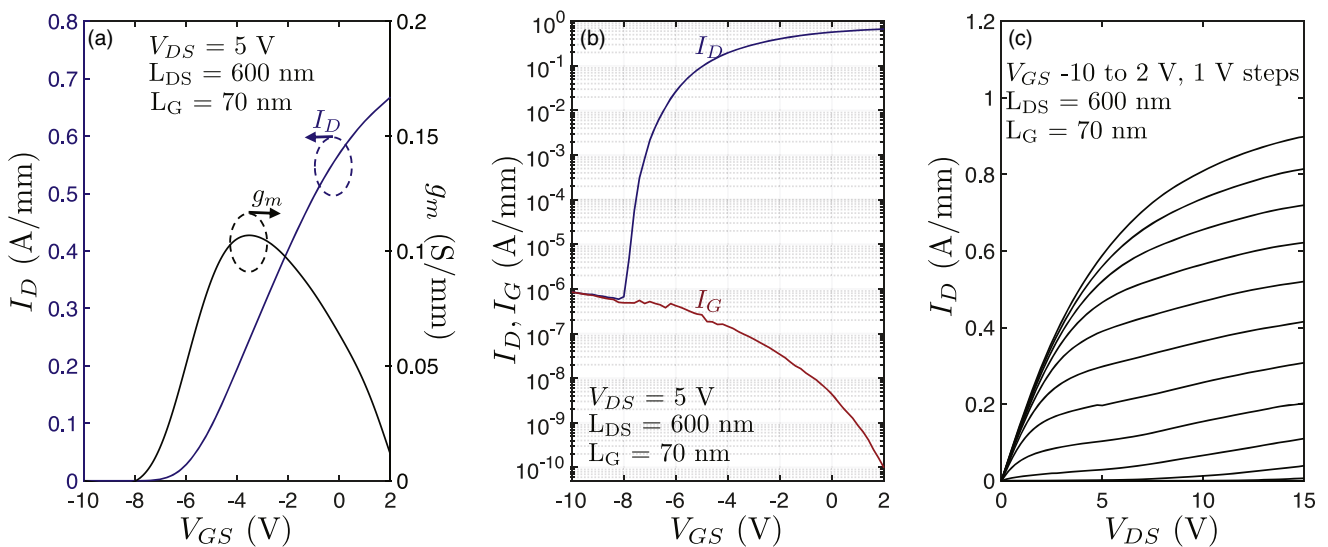


Fig. 2. DC characteristics of the AlN/Al_{0.25}Ga_{0.75}N/AlN HEMTs. The linear (a) and log (b) scale transfer characteristics, showing a peak transconductance of 0.11 S mm⁻¹ and an on/off ratio exceeding 6 orders. (c) Output characteristics demonstrating a maximum drain current of 0.9 A mm⁻¹ at a gate voltage of 2 V.

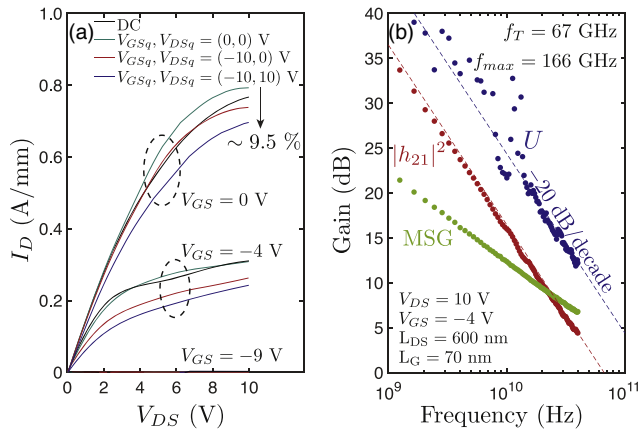


Fig. 3. (a) Pulsed $I_D V_{DS}$ measured with a 500 ns pulsed with 0.05% duty cycle at different biasing conditions shown in the plot. Maximum current collapse of 10% and moderate knee walkout were observed. (b) Small signal characteristics of a HEMT with $L_G = 70$ nm, with an extrapolated $f_T f_{max} = 67/166$ GHz at a gate and drain bias of -4 V and 10 V, respectively.

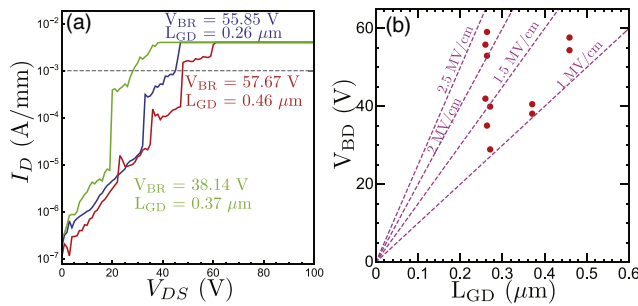


Fig. 4. Breakdown characteristics for three HEMTs with $L_{GD} = 0.26, 0.37,$ and 0.46 μm at a gate bias of -10 V. (b) Scaling of breakdown voltage as a function of L_{GD} .

function of L_{GD} , all the measured HEMTs show $E_{avg} > 1 \text{ MV cm}^{-1}$, demonstrating the potential of QW HEMTs for extremely high-power operation in RF applications. It should be noted that, however, the devices examined for the breakdown characteristics are not free of dispersion as shown in Fig. 3(a). Unless properly passivated, the top barrier surface can become negatively charged by the electrons injected from the gate during off-state, extending the depletion width and lowering the peak electric field. Therefore, surface traps may be playing a role in increasing the breakdown voltage in measured devices. In order to accurately assess the impact of the AlGaIn channel on breakdown characteristics, careful control of surface states would be necessary in the future.

A Maury load-pull system at 10 GHz was used for large signal continuous wave RF measurements. After finding the impedance for maximum output power density (P_{out}) by tuning an external load, input power was swept to measure gain, P_{out} , and power-added efficiency (PAE). CW large signal load-pull measurement was performed at class AB operation with a bias condition of $V_{DS} = 15$ V and $V_{GS} = -3$ V. As shown in Fig. 5(a), a saturation output power $P_{out} = 2 \text{ W mm}^{-1}$ is obtained at 10 GHz. The maximum PAE is measured to be $\sim 20\%$ and the power gain G_T is 5.2 dB at this condition. Further increase in PAE and P_{out} are

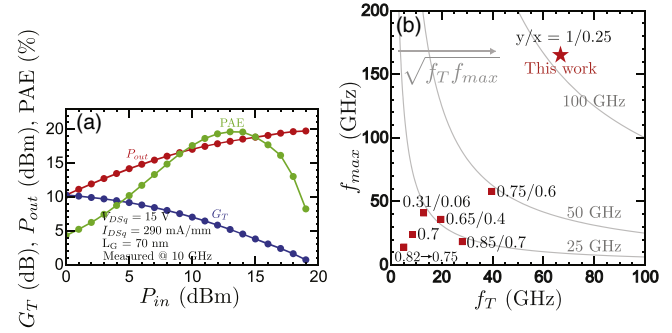


Fig. 5. (a) RF power sweep at 10 GHz at $V_{DSq}/V_{GSq} = 15/-3$ V, showing a peak PAE of 20% and maximum output power density of 2 W mm^{-1} . (b) Benchmark comparing $f_T f_{max}$ of AlGaIn channel HEMTs reported in the literature with this work. y/x indicates the Al composition in the top barrier/channel layer ($\text{Al}_y\text{Ga}_{1-y}\text{N}/\text{Al}_x\text{Ga}_{1-x}\text{N}$).^{13,14,23–26}

limited by the soft gain compression, again attributed to the surface or bulk traps.

Lastly, in Fig. 5(b), the small signal characteristics are benchmarked in terms of f_T and f_{max} against the state-of-the-art AlGaIn channel HEMTs reported in the literature. In the benchmark plot, y and x indicate the Al mole fraction in the top barrier and the channel, respectively ($\text{Al}_y\text{Ga}_{1-y}\text{N}/\text{Al}_x\text{Ga}_{1-x}\text{N}$). The $\text{AlN}/\text{Al}_{0.25}\text{Ga}_{0.75}\text{N}/\text{AlN}$ QW HEMTs presented in this study exhibited the highest speed among all other AlGaIn channel transistors, with the record high f_T/f_{max} of 67/166 GHz. This translates to the geometric mean of f_T and f_{max} exceeding 105 GHz, breaking the 100 GHz barrier for the first time for AlGaIn channel HEMTs. The high speed observed in $\text{Al}_{0.25}\text{Ga}_{0.75}\text{N}$ channel HEMTs is attributed to a low contact resistance, which has been reported to be challenging to achieve with a higher Al composition AlGaIn channel, as well as an aggressively scaled gate length and source-to-drain distance. Although the electron mobility of AlGaIn channel HEMTs is lower (consequently R_{sh} is higher) than that of GaN channel HEMTs due to alloy scattering, for RF devices the low mobility can be overcome by scaling the gate length to ensure that the carriers under the gate are velocity-saturated, while simultaneously reducing the source-to-drain distance to decrease the access resistance.

However, the contact resistance remains unaffected by the device scaling efforts due to the intrinsically lower electron affinity of a higher Al composition AlGaIn channel. This has led researchers to shift their focus from the conventional regrown n^+ -GaIn contact method via MBE or MOCVD to exploring various contact formation schemes. Some of the highlights include $R_c = 0.43 \Omega \cdot \text{mm}$ on $\text{Al}_{0.5}\text{Ga}_{0.5}\text{N}$ using regrown n^+ -GaIn prepared by pulsed sputtering deposition and $R_c = 4.3 \Omega \cdot \text{mm}$ on $\text{Al}_{0.64}\text{Ga}_{0.36}\text{N}$ using a Si-doped reverse graded $\text{Al}_x\text{Ga}_{1-x}\text{N}$ ($x = 0.87 \rightarrow 0.40$) layer.^{16,27} Despite the efforts, contact resistances reported in the literature for AlGaIn channel HEMTs with the Al mole fraction greater than 0.60 are still outside the acceptable range to outperform the GaN channel HEMTs for power amplification at high frequencies, highlighting the importance of ensuring low resistivity ohmic contacts. With proper scaling of devices, however, high Al composition AlGaIn channel HEMTs are expected to show a higher JFOM than

that reported in this study with a relatively low Al composition, once the challenges in ohmic contact formation are addressed.

In summary, highly scaled $\text{Al}_{0.25}\text{Ga}_{0.75}\text{N}$ quantum well channel HEMTs were demonstrated, showing a maximum drain current over 0.9 A mm^{-1} , a peak transconductance of 0.11 S mm^{-1} , and a record high speed $f_T/f_{\text{max}} = 67/166 \text{ GHz}$. Devices with $L_{\text{GD}} = 270 \text{ nm}$ exhibited an average breakdown field exceeding 2 MV cm^{-1} and a maximum output power density of 2 W mm^{-1} with a 20% PAE in the X-band, where the output power is mainly limited by the soft gain compression. This initial set of data suggests that AlGaN channel transistors can achieve a comparable level of gain at high frequencies to GaN channel transistors despite the lower electron mobility. This provides a clear path for transitioning into higher Al composition AlGaN channel, provided that low resistivity ohmic contacts can be ensured.

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Author contributions

E.K. and J.S. contributed equally to this work.

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